# **Titen HD®** Design Information — Concrete



#### Titen HD® Tension Strength Design Data<sup>1</sup>

There is to leave the state of												
Chamataviatia	Cumbal	Units				Nomina	I Anchor	Diamete	r, d <sub>a</sub> (in.)			
Characteristic	Symbol	Units	1/49		8	<b>%</b>	1	/2	5/	9	ą	V4
Nominal Embedment Depth	h <sub>nom</sub>	in.	15/8	21/2	21/2	31/4	31/4	4	4	51/2	51/2	61/4
		Steel S	Strength i	in Tensio	n							
Tension Resistance of Steel	N <sub>sa</sub>	lb.	5,1	5,195 10,890 20,130				130	30,	360	45,	540
Strength Reduction Factor — Steel Failure	$\phi_{sa}$	_					0.6	35 <sup>2</sup>				
Concrete Breakout Strength in Tension <sup>6,8</sup>												
Effective Embedment Depth	h <sub>ef</sub>	in.	1.19	1.94	1.77	2.40	2.35	2.99	2.97	4.24	4.22	4.86
Critical Edge Distance <sup>6</sup>	c <sub>ac</sub>	in.	3	6	211/16	35/8	39/16	41/2	41/2	6 %	6%	75/16
Effectiveness Factor — Uncracked Concrete	k <sub>uncr</sub>	_	30					24				
Effectiveness Factor — Cracked Concrete	k <sub>cr</sub>						1	7				
Modification Factor	$\Psi_{c,N}$	_					1.	.0				
Strength Reduction Factor — Concrete Breakout Failure	$\phi_{cb}$	_					0.6	35 <sup>7</sup>				
		Pullout	Strength	in Tensio	n <sup>8</sup>							
Pullout Resistance, Uncracked Concrete (f'c=2,500 psi)	N <sub>p,uncr</sub>	lb.	3	3	2,7004	3	3	3	3	9,8104	3	3
Pullout Resistance, Cracked Concrete (f'c=2,500 psi)	N <sub>p,cr</sub>	lb.	3	1,9054	1,2354	2,7004	3	3	3,2604	5,5704	6,0704	7,1954
Strength Reduction Factor — Concrete Pullout Failure	$\phi_{D}$	_					0.6	35 <sup>5</sup>				
Breakout or Pullout Strength in Tension for Seismic Applications <sup>e</sup>												
Nominal Pullout Strength for Seismic Loads (f'c=2,500 psi)	N <sub>p,eq</sub>	lb.	3	1,9054	1,2354	2,7004	3	3	3,2604	5,5704	6,0704	7,1954
Strength Reduction Factor — Breakout or Pullout Failure	$\phi_{eq}$	_	0.655									

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318 Appendix D, except as modified below.
- 2. The value of \$\phi\$ applies when the load combinations of ACI 318 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ . Anchors are considered brittle
- Pullout strength is not reported since concrete breakout controls.
- 4. Adjust the characteristic pullout resistance for other concrete compressive strengths by multiplying the tabular value by (f'c, specified / 2,500)0.5
- 5. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3(c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 6. The modification factor  $\Psi_{cp,N} = 1.0$  for cracked concrete. Otherwise, the modification factor for uncracked concrete without supplementary reinforcement to control splitting is either:

(1) 
$$\Psi_{cp,N} = 1.0 \text{ if } c_{a,min} \ge c_{ac} \text{ or (2) } \Psi_{cp,N} = \frac{c_{a,min}}{c_{ac}} \ge \frac{1.5h_{af}}{c_{ac}} \text{ if } c_{a,min} < c_{ac}$$

The modification factor,  $\Psi_{cp,N}$  is applied to the nominal concrete breakout strength,  $N_{cb}$  or  $N_{cbg}$ .

- 7. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3(c) for Condition B are met. If the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3(c) for Condition A are met, refer to Section D.4.3 to determine the appropriate value of  $\phi$ . If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 8. For sand-lightweight concrete, in lieu of ACI 318 Section D.3.6, modify the value of concrete breakout strength,  $N_{p,cr}$ ,  $N_{p,uncr}$  and  $N_{eq}$  by 0.6. All-lightweight concrete is beyond the scope of this table.
- 9. Data for 1/4" anchor is valid only for THDB25 series. Data for 1/4" anchor is valid only for THDB62 series.

## Titen HD® Shear Strength Design Data<sup>1</sup>

Characteristic	Symbol	Units				Nomina	l Anchor	Diamete	r, d <sub>a</sub> (in.)			
Giaracteristic	Буппон	Units	1/4	1/45		<b>%</b>	1	/2	5,	<b>6</b> <sup>5</sup>	3	<b>/</b> 4
Nominal Embedment Depth	h <sub>nom</sub>	in.	1%	21/2	21/2	31/4	31/4	4	4	51/2	51/2	61/4
Steel Strength in Shear												
Shear Resistance of Steel	V <sub>sa</sub>	lb.	2,020 4,460			7,4	155	10,	000	16,	840	
Strength Reduction Factor — Steel Failure	$\phi_{sa}$			$0.60^{2}$								
Concrete Breakout Strength in Shear												
Outside Diameter	da	in.	0.3	25	0.3	375	0.500		0.625		0.75	
Load Bearing Length of Anchor in Shear	$\ell_e$	in.	1.19	1.94	1.77	2.40	2.35	2.99	2.97	4.24	4.22	4.86
Strength Reduction Factor — Concrete Breakout Failure	$\phi_{cb}$	_					0.7	70⁴				
	Co	ncrete P	ryout Stre	ength in S	Shear							
Coefficient for Pryout Strength	k <sub>cp</sub>	lb.			1.0					2.0		
Strength Reduction Factor — Concrete Pryout Failure	$\phi_{\scriptscriptstyle CD}$	_					0.7	70 <sup>4</sup>				
Steel Strength in Shear for Seismic Applications												
Shear Resistance for Seismic Loads	V <sub>eq</sub>	lb.	1,695 2,855			4,790		8,000		9,3	350	
Strength Reduction Factor — Steel Failure	$\phi_{ea}$	_					0.6	60 <sup>2</sup>				

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318 Appendix D, except as modified below.
- 2. The value of  $\phi$  applies when the load combinations of ACI 318 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ . Anchors are considered brittle steel elements.
- 3. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3(c) for Condition B are met. If the load combinations of ACI 318 Section 9.2 are used, and the requirements of
- refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 4. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3(c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 5. Data for 1/4" anchor is valid only for THDB25 series. Data for 5/6" anchor is valid only for THDB62 series.
- 6. For sand-lightweight concrete, in lieu of ACI 318 Section D.3.6, modify the value

# **Mechanical** Anchors

#### Simpson Strong-Tie® Anchoring and Fastening Systems for Concrete and Masonry

# **Titen HD®** Design Information — Concrete



Titen HD® Tension and Shear Strength Design Data for the Soffit of Normal-Weight or Sand-Lightweight Concrete over Metal Deck<sup>1,6,8</sup>

IBC		<b>→</b>	
IDU	339	350 350	

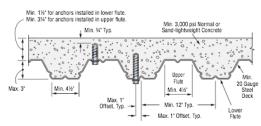
			Nominal Anchor Diameter, d <sub>a</sub> (in.)											
Characteristic	Cumbal	Symbol Units		Lower Flute					Upper Flute					
Gladacteristic	Зунион	UIIILS	Figu	ıre 2		Figu	ire 1		Figu	re 2	Figu	ire 1		
			1/	48	3	<b>6</b>	1	2	1/	48	3%	1/2		
Nominal Embedment Depth	h <sub>nom</sub>	in.	15/8	21/2	17/8	21/2	2	31/2	15/8	21/2	17/8	2		
Effective Embedment Depth	h <sub>ef</sub>	in.	1.19	1.94	1.23	1.77	1.29	2.56	1.19	1.94	1.23	1.29		
Pullout Resistance, concrete on metal deck (cracked) <sup>2,3,4</sup>	$N_{p,deck,cr}$	lb.	420	535	375	870	905	2,040	655	1,195	500	1,700		
Pullout Resistance, concrete on metal deck (uncracked) <sup>2,3,4</sup>	N <sub>p,deck,uncr</sub>	lb.	995	1,275	825	1,905	1,295	2,910	1,555	2,850	1,095	2,430		
Steel Strength in Shear, concrete on metal deck <sup>5</sup>	V <sub>sa, deck</sub>	lb.	1,335	1,745	2,240	2,395	2,435	4,430	2,010	2,420	4,180	7,145		
Steel Strength in Shear, Seismic	V <sub>sa. deck.eq</sub>	lb.	870	1,135	1,434	1,533	1,556	2,846	1,305	1,575	2,676	4,591		

- The information presented in this table is to be used in conjunction with the design criteria of ACI 318 Appendix D, except as modified below.
- Concrete compressive strength shall be 3,000 psi minimum. The characteristic pullout resistance for greater compressive strengths shall be increased by multiplying the tabular value by (f<sup>\*</sup><sub>c,specified</sub> /3,000)<sup>0.5</sup>.
- 3. For anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and roof assemblies, as shown in Figure 1 and Figure 2, calculation of the concrete breakout strength may be omitted.
- 4. In accordance with ACI 318 Section D.5.3.2, the nominal pullout strength in cracked concrete for anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and roof assemblies N<sub>p,deck,cr</sub>
- shall be substituted for  $N_{p,cr}$ . Where analysis indicates no cracking at service loads, the normal pullout strength in uncracked concrete  $N_{p,deck,uncr}$  shall be substituted for  $N_{p,uncr}$ .
- 5. In accordance with ACI 318 Section D.6.1.2(c), the shear strength for anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and roof assemblies  $V_{\rm sa,deck}$  and  $V_{\rm sa,deck,eq}$  shall be substituted for  $V_{\rm sa}$ .
- 6. Minimum edge distance to edge of panel is 2h ef-
- 7. The minimum anchor spacing along the flute must be the greater of  $3h_{\rm ef}$ , or 1.5 times the flute width.
- 8. Data for 1/4" anchor is valid only for THDB25 series.

# Titen HD® Anchor Tension and Shear Strength Design Data in the Topside of Normal-Weight Concrete or Sand-Lightweight Concrete over Metal Deck



- 1. For anchors installed in the topside of concrete-filled deck assemblies, as shown in Figures 2 and 3, the nominal concrete breakout strength of a single anchor or group of anchors in shear,  $V_{cb}$  or  $V_{cbc}$ , respectively, must be calculated in accordance with ACI 318 D.6.2, using the actual member thickness,  $h_{min,deck}$ , in the determination of  $A_{vc}$ .
- Design capacity shall be based on calculations according to values in the tables featured on pages 185 and 186.
- 3. Minimum flute depth (distance from top of flute to bottom of flute) is 1  $\frac{1}{2}$  inch (see Figures 2 and 3).
- 4. Steel deck thickness shall be minimum 20 gauge.
- Minimum concrete thickness (h<sub>min,deck</sub>) refers to concrete thickness above upper flute (see Figures 2 and 3).



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Figure 1. Installation of %" and ½" Diameter Anchors in the Soffit of Concrete over Metal Deck

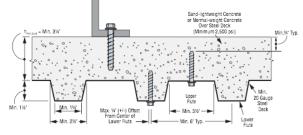


Figure 2. Installation of %" Diameter Anchors in the Topside and ¼" Diameter Anchors in the Soffit of Concrete over Metal Deck

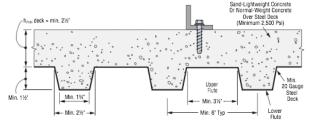


Figure 3. Installation of 1/4" Diameter Anchors in the Topside of

# **Titen HD®** Design Information — Concrete



Titen HD® Tension Design Strengths in Normal-Weight Concrete (f'c = 2,500 psi)



		Min.	Critical	Minimum	Tension Design Strength (lb.)										
Anchor Dia.   Nominal   Embed.   Depth		Concrete	Edge Distance	Edge Distance	Edge	Distances =	c <sub>ac</sub> on all si	des	Edge		= c <sub>min</sub> on one n three sides	side			
(in.)	(in ) Inmin		Cac	C <sub>min</sub>	C <sub>min</sub> SDC A		C A-B <sup>5</sup> SDC C-F <sup>6,7</sup>		SDC A-B <sup>5</sup>		SDC C-F <sup>6,7</sup>				
	()	(in.)	(in.)	(in.)	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked			
1/	15/8	31/4	3	11/2	1,265	715	950	540	660	630	495	470			
1/4	21/2	31/2	6	11/2	2,110	1,240	1,580	930	660	965	495	725			
2/	21/2	4	211/16	13/4	1,755	805	1,315	600	1,350	805	1,015	600			
3∕8	31/4	5	3%	13/4	2,900	1,755	2,175	1,315	1,810	1,290	1,360	970			
1/	31/4	5	3%16	13/4	2,810	1,990	2,105	1,495	1,765	1,265	1,325	950			
1/2	4	61/4	41/2	13/4	4,035	2,855	3,025	2,140	2,285	1,620	1,710	1,220			
5/	4	6	41/2	13/4	3,990	1,975	2,995	1,480	2,250	1,610	1,690	1,210			
5∕8	51/2	81/2	6%	13/4	6,375	3,620	4,780	2,715	3,390	2,405	2,540	1,805			
2/	51/2	83/4	6%	13/4	6,760	3,945	5,070	2,960	3,355	2,395	2,515	1,795			
3/4	61/4	10	75/16	13/4	8.355	4,675	6.265	3,510	3.990	2.835	2.990	2.125			

- 1. Tension design strengths are based on the strength design provisions of ACI 318-11 Appendix D.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.
- 4. Strength reduction factor,  $\phi$ , is based on using a load combination from ACI 318-11 Section 9.2.
- 5. The tension design strength listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 6. When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 7. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

# Titen HD® Allowable Tension Loads in Normal-Weight Concrete (f'c = 2,500 psi) — Static Load



	Manadarat	Min. Ormanda	Original Educa	Baladan Balan		Allowable Te	nsion Load (lb.)	
Anchor Dia. (in.)	Nominal Embed. Depth (in.)	Min. Concrete Thickness h <sub>min</sub> (in.)	Critical Edge Distance c <sub>ac</sub> (in.)	Minimum Edge Distance c <sub>min</sub> (in.)		= c <sub>ac</sub> on all sides	Edge Distances = and c <sub>ac</sub> on	
	()	(,	(,	(,	Uncracked	Cracked	Uncracked	Cracked
1/	1%	31/4	3	1 1/2	905	510	470	450
1/4	21/2	31/2	6	1 1/2	1,505	885	470	690
3/8	21/2	4	211/16	13/4	1,255	575	965	575
9/8	31/4	5	35/8	13/4	2,070	1,255	1,295	920
1/	31/4	5	39/16	13/4	2,005	1,420	1,260	905
1/2	4	61/4	41/2	13/4	2,880	2,040	1,630	1,155
5/	4	6	41/2	13/4	2,850	1,410	1,605	1,150
5/8	51/2	81/2	6%	13/4	4,555	2,585	2,420	1,720
2/	51/2	8¾	6%	13/4	4,830	2,820	2,395	1,710
3/4	61/4	10	75/16	13/4	5,970	3,340	2,850	2,025

- 1. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha$  = 1.4. The conversion factor  $\alpha$  is based on the load combination 1.2D + 1.6L assuming 50% dead load and 50% live load: 1.2(0.5) + 1.6(0.5) = 1.4.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.

# Titen HD® Allowable Tension Loads in Normal-Weight Concrete (f'c = 2,500 psi) — Wind Load



Anahan Dia Nominal		NI - 0	0.00-154			Allowable Ten	sion Load (lb.)	
Anchor Dia. (in.)	Nominal Embed. Depth (in.)	Min. Concrete Thickness h <sub>min</sub> (in.)	Critical Edge Distance c <sub>ac</sub> (in.)	Minimum Edge Distance c <sub>min</sub> (in.)	Edge Distances	= c <sub>ac</sub> on all sides	Edge Distances = and c <sub>ac</sub> on t	
	(,	(,	(,	(,	Uncracked	Cracked	Uncracked	Cracked
17.	1%	31/4	3	11/2	760	430	395	380
1/4	21/2	31/2	6	11/2	1,265	745	395	580
3∕8	21/2	4	211/16	13/4	1,055	485	810	485
98	31/4	5	3%	13/4	1,740	1,055	1,085	775
14	31/4	5	39/16	1¾	1,685	1,195	1,060	760
1/2	4	61/4	41/2	13/4	2,420	1,715	1,370	970
5/-	4	6	41/2	13/4	2,395	1,185	1,350	965
5/8	5½	81/2	6%	13/4	3,825	2,170	2,035	1,445
3/4	51/2	8¾	6%	1¾	4,055	2,365	2,015	1,435
9/4	61/4	10	75/16	1¾	5,015	2,805	2,395	1,700

- 1. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of α = 1.67. The conversion factor α is based on the load combination assuming 100% wind load.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.

# Titen HD® Design Information — Concrete



Titen HD® Allowable Tension Loads in Normal-Weight Concrete ( $f'_{c} = 2,500 \text{ psi}$ ) — Seismic Load

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		Min.	Critical	Minimum			Al	lowable Ter	ision Load (lb	.)		
Anchor Dia.	Nominal Embed.	nbed. Concrete		Edge	Edge	Distances	= c <sub>ac</sub> on all s	ides	Edge		c <sub>min</sub> on one three sides	side
(in.)	Depth (in.)	ės ninin	C <sub>ac</sub> (in.)	c <sub>min</sub> (in.)	SDC	A-B⁴	SDC (	C-F <sup>5,6</sup>	SDC A-B <sup>4</sup>		SDC C-F <sup>5,6</sup>	
	(in.)		(in.)	(in.)	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked
1/	1%	31/4	3	1½	885	500	665	380	460	440	345	330
1/4	21/2	31/2	6	11/2	1,475	870	1,105	650	460	675	345	510
2/	21/2	4	211/16	13/4	1,230	565	920	420	945	565	710	420
3/8	31/4	5	35/8	13/4	2,030	1,230	1,525	920	1,265	905	950	680
1/	31/4	5	3%16	13/4	1,965	1,395	1,475	1,045	1,235	885	930	665
1/2	4	61/4	41/2	13/4	2,825	2,000	2,120	1,500	1,600	1,135	1,195	855
E/	4	6	41/2	13/4	2,795	1,385	2,095	1,035	1,575	1,125	1,185	845
5/8	51/2	81/2	6%	13/4	4,465	2,535	3,345	1,900	2,375	1,685	1,780	1,265
2/	51/2	8¾	6%	13/4	4,730	2,760	3,550	2,070	2,350	1,675	1,760	1,255
3/4	61/4	10	75/16	13/4	5.850	3,275	4.385	2,455	2,795	1.985	2.095	1,490

<sup>1.</sup> Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha = \frac{1}{2}$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% seismic load.

<sup>2.</sup> Tabulated values are for a single anchor with no influence of another anchor.

<sup>3.</sup> Interpolation between embedment depths is not permitted.

<sup>4.</sup> The allowable tension load listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.

<sup>5.</sup> When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.

<sup>6.</sup> Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

# **Titen HD®** Design Information — Concrete



Titen HD® Tension Design Strengths in Soffit of Normal-Weight or Sand-Lightweight Concrete-Filled Profile Steel Deck Assemblies (f'<sub>c</sub> = 3,000 psi)



		Minimum End			Te	nsion Desig	n Strength (lb	l.)		
Anchor Dia.	Nominal Embed. Depth			Lowe	r Flute		Upper Flute			
(in.) Embed. Depar		h Distance c <sub>min</sub> (in.)	SDC A-B <sup>5</sup>		SDC C-F <sup>6,7</sup>		SDC A-B <sup>5</sup>		SDC	C-F <sup>6,7</sup>
			Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked
1/	15%	2 1/2	645	275	485	205	1,010	425	760	320
1/4	21/2	4	830	350	620	260	1,855	775	1,390	585
3/-	11/8	21/2	535	245	400	185	710	325	535	245
3/8	21/2	3%	1,240	565	930	425	_	_	_	_
1/2	2	2 %	840	590	630	440	1,580	1,105	1,185	830
72	31/2	51/4	1,890	1,325	1,420	995	_	_	_	_

- 1. Tension design strengths are based on the strength design provisions of ACI 318-11 Appendix D.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.
- 4. Strength reduction factor,  $\phi$ , is based on using a load combination from ACI 318-11 Section 9.2.
- 5. The tension design strength listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 6. When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 7. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.
- 8. Installation must comply with Figure 1 on page 187.

# Titen HD® Allowable Tension Loads in Soffit of Normal-Weight or Sand-Lightweight Concrete-Filled Profile Steel Deck Assemblies (f'<sub>c</sub> = 3,000 psi) — Static Load



Analon Blo	Nominal Embed.		Allowable Tension Load (lb.)							
Anchor Dia. (in.)	Depth	Distance c <sub>min</sub>	Lowe	r Flute	Upper Flute					
(111.)	(in.)	(in.)	Uncracked	Cracked	Uncracked	Cracked				
1/	15/8	21/2	460	195	720	305				
1/4	21/2	4	595	250	1,325	555				
2/	17/8	21/2	380	175	505	230				
3∕8	21/2	3%	885	405	_	_				
1/2	2	2%	600	420	1,130	790				
	31/2	51/4	1,350	945	_	_				

- Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of α = 1.4.
   The conversion factor α is based on the load combination 1.2D + 1.6L assuming 50% dead load and 50% live load: 1.2(0.5) + 1.6(0.5) = 1.4.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.
- 4. Installation must comply with Figure 1 on page 187.

# Titen HD® Allowable Tension Loads in Soffit of Normal-Weight or Sand-Lightweight Concrete-Filled Profile Steel Deck Assemblies ( $f'_c = 3,000 \text{ psi}$ ) — Wind Load



Annaham Dia	Nominal Embed. Minimum End		Allowable Tension Load (lb.)						
Anchor Dia. (in.)	Depth	Distance c <sub>min</sub>	Distance c <sub>min</sub> Lower Flute			Flute			
(111.)	(in.)	(in.)	Uncracked	Cracked	Uncracked	Cracked			
1/4	1%	21/2	385	165	605	255			
74	21/2	4	500	210	1,115	465			
3∕8	1%	21/2	320	145	425	195			
%8	21/2	3%	745	340	_	_			
14	2	25/8	505	355	950	665			
1/2	31/2	51/4	1,135	795	_	_			

- Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D
  using a conversion factor of α = 16.5. The conversion factor α is based on the load combination assuming 100% wind load.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted
- 4. Installation must comply with Figure 1 on page 187.

# **Titen HD®** Design Information — Concrete



Titen HD® Allowable Tension Loads in Soffit of Normal-Weight or Sand-Lightweight Concrete-Filled Profile Steel Deck Assemblies (f'c = 3,000 psi) — Seismic Load

	IBC		~~
Inner	Flute		
эррог		C-F <sup>5,6</sup>	
ced	Uncracked	Crac	cked

IDC 1 -\*

	Nominal	Minimum			Al	lowable Ter	ision Load (lb	l.)			
Anchor Dia.	Embed. Depth (in.)	End Distance		Lowe	r Flute			Upper Flute			
(in.)		C <sub>min</sub> (in.)	SDC A-B <sup>4</sup>		SDC C-F <sup>5,6</sup>		SDC A-B4		SDC C-F <sup>5,6</sup>		
			Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	
1/.	15/8	2 1/2	450	195	340	145	705	300	530	225	
1/4	21/2	4	580	245	435	180	1300	545	975	410	
3/8	1%	21/2	375	170	280	130	495	230	375	170	
98	21/2	3 %	870	395	650	300	_	_	_	_	
1/2	2	2 1/8	590	415	440	310	1105	775	830	580	
	31/2	51/4	1325	930	995	695	_	_	_	_	

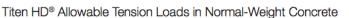
- 1. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha = \%$ .7 = 1.43. The conversion factor  $\alpha$  is based on the load combination assuming 100% seismic load.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.
- 4. The allowable tension load listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 5. When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 6. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.
- 7. Installation must comply with Figure 1 on page 187.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

#### Simpson Strong-Tie® Anchoring and Fastening Systems for Concrete and Masonry

# **Titen HD®** Design Information — Concrete





IBC	1	

			Order of Educa	Tension Load							
Size (in.)	Drill Bit Dia.	Embed. Depth in.	Critical Edge Dist. in.	Critical Spacing in.	f' <sub>c</sub> ≥2,000	psi (13.8 MP	a Concrete)	f' <sub>c</sub> ≥3,000 psi (20.7 MPa Concrete)	f' <sub>c</sub> ≥4,000	psi (27.6 MP	a Concrete)
(111.)	(in.)	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)
		<b>1½</b> (38)	<b>6</b> (152)	<b>4</b> (102)	<b>2,070</b> (9.2)	_	<b>520</b> (2.3)	<b>635</b> (2.8)	<b>2,974</b> (13.2)	_	<b>745</b> (3.3)
<sup>3</sup> / <sub>8</sub> (9.5)	(9.5) 9/8 (7	<b>2¾</b> (70)	3	6	<b>4,297</b> (19.1)	_	<b>1,075</b> (4.8)	<b>1,315</b> (5.8)	<b>6,204</b> (27.6)	_	<b>1,550</b> (6.9)
<b>3¾</b> (95)	(76)	(152)	<b>7,087</b> (31.5)	<b>347</b> (1.5)	<b>1,770</b> (7.9)	<b>2,115</b> (9.4)	<b>9,820</b> (43.7)	<b>1,434</b> (6.4)	<b>2,455</b> (10.9)		
		<b>2¾</b> (70)			<b>4,610</b> (20.5)	_	<b>1,155</b> (5.1)	<b>1,400</b> (6.2)	<b>6,580</b> (29.3)	_	<b>1,645</b> (7.3)
½ (12.7)	1/2	<b>3</b> % (92)	<b>4</b> (102)	<b>8</b> (203)	<b>7,413</b> (33.0)	<b>412</b> (1.8)	<b>1,855</b> (8.3)	<b>2,270</b> (10.1)	<b>10,742</b> (47.8)	<b>600</b> (2.7)	<b>2,685</b> (11.9)
		<b>5¾</b> (146)			<b>10,278</b> (45.7)	<b>297</b> (1.3)	<b>2,570</b> (11.4)	<b>3,240</b> (14.4)	<b>15,640</b> (69.6)	<b>2,341</b> (10.4)	<b>3,910</b> (17.4)
		<b>2³/4</b> (70)		10	<b>4,610</b> (20.5)	_	<b>1,155</b> (5.1)	<b>1,400</b> (6.2)	<b>6,580</b> (29.3)	_	<b>1,645</b> (7.3)
5% (15.9)	5/8	<b>4½</b> (105)	<b>5</b> (127)	10 (254)	8,742 (38.9)	<b>615</b> (2.7)	<b>2,185</b> (9.7)	<b>2,630</b> (11.7)	<b>12,286</b> (54.7)	<b>1,604</b> (7.1)	<b>3,070</b> (13.7)
		<b>5¾</b> (146)			<b>12,953</b> (57.6)	<b>1,764</b> (7.8)	<b>3,240</b> (14.4)	<b>3,955</b> (17.6)	<b>18,680</b> (83.1)	_	<b>4,670</b> (20.8)
		<b>2¾</b> (70)			<b>4,674</b> (20.8)	<u> </u>	<b>1,170</b> (5.2)	<b>1,405</b> (6.3)	<b>6,580</b> (29.3)	_	<b>1,645</b> (7.3)
<sup>3</sup> / <sub>4</sub> (19.1)	3/4	<b>4</b> 5/8 (117)	<b>6</b> (152)	<b>12</b> (305)	<b>10,340</b> (46.0)	<b>1,096</b> (4.9)	<b>2,585</b> (11.5)	<b>3,470</b> (15.4)	<b>17,426</b> (77.5)	<b>1,591</b> (7.1)	<b>4,355</b> (19.4)
		<b>5¾</b> (146)			<b>13,765</b> (61.2)	<b>1,016</b> (4.5)	<b>3,440</b> (15.3)	<b>4,055</b> (18.0)	<b>18,680</b> (83.1)	<b>1,743</b> (7.8)	<b>4,670</b> (20.8)

- 1. The allowable loads listed are based on a safety factor of 4.0.
- 2. Refer to allowable load-adjustment factors for spacing and edge distance on pages 198 and 199.
- 3. The minimum concrete thickness is 11/2 times the embedment depth.
- 4. Tension and shear loads for the Titen HD anchor may be combined using the elliptical interaction equation (n=5/s). Allowable load may be interpolated for concrete compressive strengths between 2,000 psi and 4,000 psi.

## Titen HD® Allowable Shear Loads in Normal-Weight Concrete



				Shear Load Shear Load																
Size (in.)	Drill Bit	Embed. Depth in. (mm)	Critical Edge Dist. in. (mm)	Critical Spacing in. (mm)	f' <sub>c</sub> ≥2,000 psi (13.8 MPa Concrete)			f' <sub>c</sub> ≥3,000 psi (20.7 MPa Concrete)	f' <sub>c</sub> ≥4,000	psi (27.6 MP	a Concrete)									
	Dia. (III.)	(11111)	Dist. III. (IIIII)		Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)									
		<b>1½</b> (38)	<b>6</b> (152)	<b>4</b> (102)	<b>2,912</b> (13.0)	_	<b>730</b> (3.2)	<b>825</b> (3.7)	<b>3,668</b> (16.3)	_	<b>915</b> (4.1)									
3/8 (9.5)		<b>2¾</b> (70)	41/2	6	<b>6,353</b> (28.3)	_	<b>1,585</b> (7.1)	<b>1,665</b> (7.4)	_	_	<b>1,740</b> (7.7)									
(212)	<b>3¾</b> (95)	(114)	(152)	<b>6,377</b> (28.4)	<b>1,006</b> (4.5)	<b>1,595</b> (7.1)	<b>1,670</b> (7.4)	_	_	<b>1,740</b> (7.7)										
	23/4 (70) 1/2 1/2 33/6 (12.7) 1/2 (92)		<b>6</b> (152)					<b>6,435</b> (28.6)	<u> </u>	<b>1,605</b> (7.1)	<b>2,050</b> (9.1)	<b>9,987</b> (44.4)	_	<b>2,495</b> (7.8)						
½ (12.7)					<b>8</b> (203)	<b>9,324</b> (41.5)	<b>1,285</b> (5.7)	<b>2,330</b> (10.4)	<b>2,795</b> (12.4)	<b>13,027</b> (57.9)	<b>597</b> (2.7)	<b>3,255</b> (14.5)								
		<b>5</b> <sup>3</sup> ⁄ <sub>4</sub> (146)			<b>11,319</b> (50.3)	<b>1,245</b> (5.5)	<b>2,830</b> (12.6)	<b>3,045</b> (13.5)	_	_	<b>3,255</b> (14.5)									
		<b>2¾</b> (70)	<b>7½</b> (191)	<b>7½</b> (191)										<b>7,745</b> (34.5)	_	<b>1,940</b> (8.6)	<b>2,220</b> (9.9)	<b>9,987</b> (44.4)	_	<b>2,495</b> (7.8)
<b>5</b> % (15.9)	5/8	<b>4</b> 1/ <sub>8</sub> (105)				10 (254)	<b>8,706</b> (38.7)	<b>1,830</b> (8.1)	<b>2,175</b> (9.7)	<b>3,415</b> (15.2)	18,607 (82.8)	<b>1,650</b> (7.3)	<b>4,650</b> (20.7)							
		<b>5</b> <sup>3</sup> ⁄ <sub>4</sub> (146)			<b>12,498</b> (55.6)	<b>2,227</b> (9.9)	<b>3,125</b> (13.9)	<b>3,890</b> (17.3)	_	_	<b>4,650</b> (20.7)									
		<b>2¾</b> (70)	<b>9</b> (229)								<b>7,832</b> (34.8)	_	<b>1,960</b> (8.7)	<b>2,415</b> (10.7)	<b>11,460</b> (51.0)	_	<b>2,865</b> (12.7)			
3/4 (19.1)	3/4	<b>4</b> 5% (117)		<b>12</b> (305)	<b>11,222</b> (49.9)	<b>2,900</b> (12.9)	<b>2,805</b> (12.5)	<b>4,490</b> (20.0)	<b>24,680</b> (109.8)	<b>2,368</b> (10.5)	<b>6,170</b> (27.4)									
(10.1)		<b>5¾</b> (146)			<b>19,793</b> (88.0)	<b>3,547</b> (15.8)	<b>4,950</b> (22.0)	<b>5,560</b> (24.7)	<b>24,680</b> (109.8)	<b>795</b> (3.5)	<b>6,170</b> (27.4)									

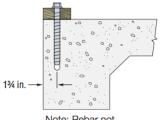
- 1. The allowable loads listed are based on a safefy factor of 4.0.
- 2. Refer to allowable load-adjustment factors for spacing and edge distance on pages 198 and 199.
- 4. Tension and shear loads for the Titen HD anchor may be combined using the elliptical interaction equation (n=%).

# **Titen HD®** Design Information — Concrete

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Titen HD® Allowable Shear Loads in Normal-Weight Concrete, Load Applied Parallel to Concrete Edge

	.ppou 1	C. C.IOI L	o Concre			She	ar Load Base	d on	
Size	Drill Bit	Embed.	Minimum Edge	Minimum End Dist. in. (mm)	Minimum Spacing	Concrete Edge Distance			
in.	Dia.	Depth in.	Dist. in. (mm)		Dist. in. (mm)	f' <sub>c</sub> ≥ 2,500	psi (17.2 MP	a) Concrete	
(mm)	in.	(mm)				Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	
		<b>2¾</b> (70)				<b>4,660</b> (20.7)	<b>575</b> (2.6)	<b>1,165</b> (5.2)	
1/2 1/2	<b>31/4</b> (83)	1¾	8	8	_	_	<b>1,530</b> (6.8)		
(12.7)	//2	<b>3½</b> (89)	(45)	(203)	(203)	<b>6,840</b> (30.4)	<b>860</b> (3.8)	<b>1,710</b> (7.6)	
		<b>4½</b> (114)				<b>7,800</b> (34.7)	<b>300</b> (1.3)	<b>1,950</b> (8.7)	
		<b>2¾</b> (70)				<b>4,820</b> (21.4)	<b>585</b> (2.6)	<b>1,205</b> (5.3)	
5% (15.9)	5/8	<b>31/4</b> (83)	<b>1¾</b> (45)	<b>10</b> (254)	10 (254)	_	_	<b>1,580</b> (7.0)	
		<b>3½</b> (89)				<b>7,060</b> (31.4)	<b>1,284</b> (5.7)	<b>1,765</b> (7.9)	



Note: Rebar not shown for clarity.

- 1. The allowable loads listed are based on a safety factor of 4.0.
- 2. The minimum concrete thickness is 11/2 times the embedment depth.

# Titen HD® Allowable Tension Loads in Normal-Weight Concrete Stemwall



- 1. The allowable loads are based on a safety factor of 4.0.
- 2. The minimum anchor spacing is 15 inches.
- 3. The minimum concrete thickness (depth) is 12 inches.
- Allowable loads may be interpolated for compressive strengths between 2,500 and 4,500 psi.

# Titen HD® Allowable Tension Loads in Normal-Weight Concrete, Load Applied at 60° Angle to Horizontal for Tilt-Up Wall Braces

		Embed.	Tension Applied at 60 degrees to Horizontal  f' <sub>c</sub> ≥ 2,500 psi (17.2 MPa) Concrete					
Size in. (mm)	Drill Bit Dia. in.	Depth in.						
		(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allow. lb. (kN)			
5% (15.9)	5/8	<b>5</b> (127)	<b>13,420</b> (59.7)	<b>1,273</b> (5.7)	<b>3,355</b> (14.9)			
3/4 (19.1)	3/4	<b>5</b> (127)	<b>15,180</b> (67.5)	<b>968</b> (4.3)	<b>3,795</b> (16.9)			

- 1. The allowable loads are based on a safety factor of 4.0.
- Anchor must be installed into a concrete floor slab, footing, or deadman with sufficient area, weight, and strength to resist the anchorage load.
- Titen HD® has been qualified for temporary outdoor use of up to 90 days through testing for this application.



The Titen HD® screw anchor ¾" x 6" and ¾" x 7" (models THDT75600H and THD75700H) have a 1" section under the head that is unthreaded to allow installation into tilt-up wall braces.

# **Titen HD®** Design Information — Concrete

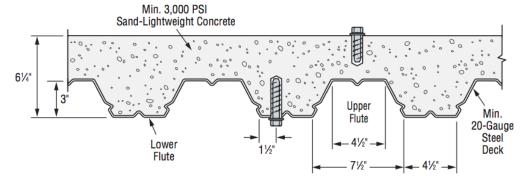


Titen HD® Allowable Tension and Shear Loads in Sand-Lightweight Concrete over Metal Deck

IBC		<b>→</b>	
	853 858	200	

					Inst	tall in Concrete	(see Figure bel	low)	Install t	hrough Metal D	eck (see Figure	e below)		
Size	Drill	Embed.	Critical Edge	Critical Spacing	Tensio	n Load	Shea	r Load	Tension Load		Shear Load			
in. (mm)	Bit Dia. in.	Depth in.	Dist. in.	Dist. in.	f' <sub>c</sub> ≥ 3,000 psi (20.7 MPa) Lightweight Concrete			f' <sub>c</sub> ≥ 3,000 psi (20.7 MPa) Lightweight Concrete		f' <sub>c</sub> ≥ 3,000 psi (20.7 MPa) Lightweight Concrete		si (20.7 MPa) nt Concrete		
	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lbs. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)			
3/8	2/	<b>2¾</b> (70)	6	6	<b>2,560</b> (11.4)	<b>640</b> (2.8)	<b>4,240</b> (18.9)	<b>1,060</b> (4.7)	_	_	_	_		
3 <b>%</b> (9.5)	3 (15) (76)	(152)	2) (152)	_	_	_	_	<b>5,420</b> (24.1)	<b>1,355</b> (6.0)	<b>4,100</b> (18.2)	<b>1,025</b> (4.6)			
1/2	1/2	<b>2¾</b> (70)	8			8	<b>3,040</b> (13.5)	<b>760</b> (3.4)	<b>6,380</b> (28.4)	<b>1,595</b> (7.1)	_	_	_	_
(12.7)	1/2	<b>4</b> (102)	(203)	(203)	_	_	_	_	<b>7,020</b> (31.2)	<b>1,755</b> (7.8)	<b>6,840</b> (30.4)	<b>1,710</b> (7.6)		
5/8	5/	<b>2¾</b> (70)	10 10		<b>3,100</b> (13.8)	<b>775</b> (3.4)	<b>6,380</b> (28.4)	<b>1,595</b> (7.1)	_	_	_	_		
(15.9) 5/8	<b>5</b> (127)	(254)	(254)	_	_	_	_	<b>8,940</b> (39.8)	<b>2,235</b> (9.9)	<b>10,700</b> (47.6)	<b>2,675</b> (11.9)			

- 1. The allowable loads listed are based on a safety factor of 4.0.
- 2. Allowable loads for anchors installed in the lower flute of the steel deck are for flutes with a trapezoidal profile with a depth of 3 inches, and a width varying from 4½ inches at the bottom to 7½ inches at the top. The spacing of the flutes is 12 inches. The metal deck must be minimum 20-gauge with a minimum yield strength of 38 ksi and minimum ultimate strength of 45 ksi.
- 3. Anchors may be installed off-center in the lower flute (up to 11/2" from the edge of the lower flute) without a load reduction.
- 4.100% of the allowable load is permitted at critical edge distance and critical spacing. Testing at smaller edge distances and spacings has not been performed.



Titen HD® screw anchor installed in the top and bottom of a structural sand-lightweight-concrete and metal-deck assembly

# **Titen HD®** Design Information — Masonry



Titen HD® Allowable Tension and Shear Loads in 8" Lightweight, Medium-Weight and Normal-Weight Grout-Filled CMU

000.												
Size	Drill	Min. Embed.	Critical Edge	Critical End Dist. in. (mm)	End Spacing Dist. Dist. in.	Values for 8-inch Lightweight, Medium-Weight or Normal-Weight Grout-Filled CMU						
in.	Bit Dia.	Depth	Dist.			Tensio	n Load	Shear	r Load			
(mm)	in.	in. (mm)	in. (mm)			Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)			
	Anchor Installed in the Face of the CMU Wall (See Figure 4)											
3/8 (9.5)	3/8	<b>2¾</b> (70)	<b>12</b> (305)	<b>12</b> (305)	<b>6</b> (152)	<b>2,390</b> (10.6)	<b>480</b> (2.1)	<b>4,340</b> (19.3)	<b>870</b> (3.9)			
½ (12.7)	1/2	<b>3½</b> (89)	<b>12</b> (305)	<b>12</b> (305)	<b>8</b> (203)	<b>3,440</b> (15.3)	<b>690</b> (3.1)	<b>6,920</b> (30.8)	<b>1,385</b> (6.2)			
<b>5%</b> (15.9)	5/8	<b>4½</b> (114)	<b>12</b> (305)	<b>12</b> (305)	<b>10</b> (254)	<b>5,300</b> (23.6)	<b>1,060</b> (4.7)	<b>10,420</b> (46.4)	<b>2,085</b> (9.3)			
3/ <sub>4</sub> (19.1)	3/4	<b>5½</b> (140)	<b>12</b> (305)	<b>12</b> (305)	<b>12</b> (305)	<b>7,990</b> (35.5)	<b>1,600</b> (7.1)	<b>15,000</b> (66.7)	<b>3,000</b> (13.3)			

- 1. The tabulated allowable loads are based on a safety factor of 5.0 for installations under the IBC and IRC.
- 2. Values for 8-inch-wide, lightweight, medium-weight and normal-weight concrete masonry units.
- 3. The masonry units must be fully grouted.
- 4. The minimum specified compressive strength of masonry, f'm, at 28 days is 1,500 psi.
- 5. Embedment depth is measured from the outside face of the concrete masonry unit.
- Allowable loads may be increased 331/4% for short-term loading due to wind or seismic forces where permitted by code.
- Grout-filled CMU wall design must satisfy applicable design standards and be capable of withstanding applied loads.
- 8. Refer to allowable load-adjustment factors for spacing and edge distance on page 200.

4' minimum edge distance (see load lable)
Installation in this area for reduced allowable load capacity

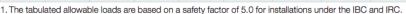
4' minimum end distance (see load table)

Installation in this area for full allowable load capacity

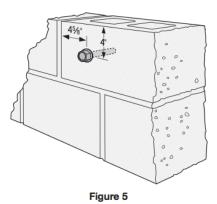
Figure 4. Shaded Area = Placement for Full and Reduced Allowable Load Capacity in Grout-Filled CMU

# Titen HD® Allowable Tension and Shear Loads in 8" Lightweight, Medium-Weight and Normal-Weight Hollow CMU

O!	Drill	Embed.	Min.	Edge End Dist. Dist.	8-inch Hollow CMU Loads Based on CMU Strength					
Size in. (mm)	Bit Dia.	Depth <sup>4</sup> in.			Tension Load		Shear Load			
in.	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate Ib. (kN)	Allowable lb. (kN)			
	Anchor Installed in Face Shell (See Figure 5)									
3/8 (9.5)	3∕8	<b>1</b> 3/4 (45)	<b>4</b> (102)	<b>45</b> /8 (117)	<b>720</b> (3.2)	<b>145</b> (0.6)	<b>1,240</b> (5.5)	<b>250</b> (1.1)		
½ (12.7)	1/2	<b>1</b> 3/4 (45)	<b>4</b> (102)	<b>4</b> 5/8 (117)	<b>760</b> (3.4)	<b>150</b> (0.7)	<b>1,240</b> (5.5)	<b>250</b> (1.1)		
<b>5⁄8</b> (15.9)	5/8	<b>1</b> 3/4 (45)	<b>4</b> (102)	<b>4</b> 5/8 (117)	<b>800</b> (3.6)	<b>160</b> (0.7)	<b>1,240</b> (5.5)	<b>250</b> (1.1)		
3/4 (19.1)	3/4	<b>13/4</b> (45)	<b>4</b> (102)	<b>4</b> 5/8 (117)	<b>880</b> (3.9)	<b>175</b> (0.8)	<b>1,240</b> (5.5)	<b>250</b> (1.1)		



- 2. Values for 8-inch-wide, lightweight, medium-weight and normal-weight concrete masonry units.
- 3. The minimum specified compressive strength of masonry, f'm, at 28 days is 1,500 psi.
- 4. Embedment depth is measured from the outside face of the concrete masonry unit and is based on the anchor being embedded an additional ½" through 1½" thick face shell.
- 5. Allowable loads may not be increased for short-term loading due to wind or seismic forces. CMU wall design must satisfy applicable design standards and be capable of withstanding applied loads.
- 6. Do not use impact wrenches to install in hollow CMU.
- 7. Set drill to rotation-only mode when drilling into hollow CMU.



# **Titen HD®** Design Information — Masonry



Titen  ${\rm HD^{\otimes}}$  Allowable Tension and Shear Loads in 8" Lightweight, Medium-Weight and Normal-Weight Grout-Filled CMU Stemwall

	Drill	Embed.	Min.		Critical	8-inch Grout-Filled CMU Allowable Loads Based on CMU Strength									
Size in.	Bit Dia.	Depth	Dist. Dist.		Spacing Dist.	Ten	sion	Shear Pe	rp. to Edge	Shear Para	illel to Edge				
(mm)	in.			(mm)	in. in. in. (mm)				in. (mm)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)
			An	chor Ins	talled in Ce	ell Opening o	r Web (Top o	f Wall) (See	Figure 6)						
½ (12.7)	1/2	<b>4½</b> (114)	<b>13/4</b> (45)	<b>8</b> (203)	<b>8</b> (203)	<b>2,860</b> (12.7)	<b>570</b> (2.5)	<b>800</b> (3.6)	<b>160</b> (0.7)	<b>2,920</b> (13.0)	<b>585</b> (2.6)				
5/8 (15.9)	5/8	<b>4½</b> (114)	<b>13/4</b> (45)	<b>10</b> (254)	<b>10</b> (254)	<b>2,860</b> (12.7)	<b>570</b> (2.5)	<b>800</b> (3.6)	<b>160</b> (0.7)	<b>3,380</b> (15.0)	<b>675</b> (3.0)				

- 1. The tabulated allowable loads are based on a safety factor of 5.0 for installations under the IBC and IRC.
- 2. Values are for 8-inch-wide, lightweight, medium-weight and normal-weight concrete masonry units.
- 3. The masonry units must be fully grouted.
- 4. The minimum specified compressive strength of masonry,  $f'_{\it m}$ , at 28 days is 1,500 psi.
- 5. Allowable loads may be increased 331/3% for short-term loading due to wind or seismic forces where permitted by code.
- 6. Grout-filled CMU wall design must satisfy applicable design standards and be capable of withstanding applied design loads.
- 7. Loads are based on anchor installed in either the web or grout-filled cell opening in the top of wall.

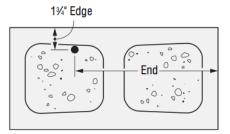


Figure 6. Anchor Installed in top of wall

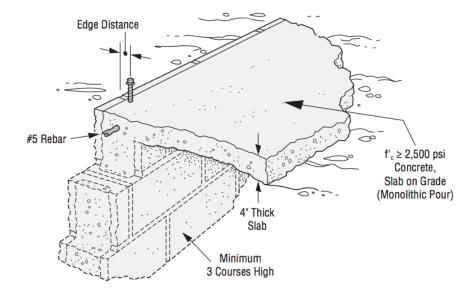
# Titen HD® Design Information — Masonry



Titen HD® Allowable Tension Loads for 8" Lightweight, Medium-Weight and Normal-Weight CMU Chair Blocks Filled with Normal-Weight Concrete

TTOTTICE TTO	Jigini Olvio (	Dirair Biooria	T IIIOG WIGH	TTOTTION TTO	grit corioroto			
Size in.	Drill Bit Dia.	Min. Embed. Depth in.	Min. Edge Dist. in.	Critical Spacing in.	8-inch Concrete-Filled CMU Chair Block Allowable Tension Loads Based on CMU Strength			
(mm)	(in.)	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Allowable lb. (kN)		
		<b>2</b> % (60)	<b>1¾</b> (44)	<b>9½</b> (241)	<b>3,175</b> (14.1)	<b>635</b> (2.8)		
<b>3/6</b> (9.5)	3∕8	<b>3</b> % (86)	<b>1¾</b> (44)	<b>13½</b> (343)	<b>5,175</b> (23.0)	<b>1,035</b> (4.6)		
		<b>5</b> (127)	<b>21/4</b> (57)	<b>20</b> (508)	<b>10,584</b> (47.1)	<b>2,115</b> (9.4)		
1/2	1/2	<b>8</b> (203)	<b>21/4</b> (57)	<b>32</b> (813)	<b>13,722</b> (61.0)	<b>2,754</b> (12.2)		
(12.7)	72	<b>10</b> (254)	<b>21/4</b> (57)	<b>40</b> (1016)	<b>16,630</b> (74.0)	<b>3,325</b> (14.8)		
5/8	5/	<b>5½</b> (140)	13/4 (44)	<b>22</b> (559)	<b>9,025</b> (40.1)	<b>1,805</b> (8.1)		
(15.9)	5/8	<b>12</b> (305)	<b>21/4</b> (57)	<b>48</b> (1219)	<b>18,104</b> (80.5)	<b>3,620</b> (16.1)		

- 1. The tabulated allowable loads are based on a safety factor of 5.0.
- 2. Values are for 8-inch-wide concrete masonry units (CMU) filled with concrete, with minimum compressive strength of 2,500 psi and poured monolithically with the floor slab.
- 3. Center #5 rebar in CMU cell and concrete slab as shown in the illustration below.



# Titen HD® Design Information — Concrete



Load Adjustment Factors for Titen HD® Anchors in Normal-Weight Concrete: Edge Distance, Tension and Shear Loads

#### How to use these charts:

- 1. The following tables are for reduced edge distance.
- 2. Locate the anchor size to be used for either a tension and/or shear load application.
- Locate the anchor embedment (E) used for either a tension and/or shear load application.
- 4. Locate the edge distance ( $c_{act}$ ) at which the anchor is to be installed.
- The load adjustment factor (f<sub>c</sub>) is the intersection of the row and column.
- 6. Multiply the allowable load by the applicable load adjustment factor(s).
- 7. Reduction factors for multiple edges are multiplied together.

$\Box$ daa	Distance	Toncion	/ <del>f</del> \
Luue	Distaile	161121011	Ucl

	Dia.	3/8				1/2			5/8			3/4		
Edge	E	11/2	23/4	33/4	23/4	3%	53/4	23/4	41/8	53/4	23/4	45/8	53/4	
Dist.	Ccr	6	3	3	4	4	4	5	5	5	6	6	6	
C <sub>act</sub> (in.)	Cmin	6	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	
(111.)	f <sub>cmin</sub>	1.00	0.83	0.73	0.67	0.57	0.73	0.67	0.57	0.59	0.67	0.48	0.58	
13/4			0.83	0.73	0.67	0.57	0.73	0.67	0.57	0.59	0.67	0.48	0.58	
2			0.86	0.78	0.71	0.62	0.76	0.70	0.60	0.62	0.69	0.51	0.60	
21/4			0.90	0.84	0.74	0.67	0.79	0.72	0.64	0.65	0.71	0.54	0.63	
21/2			0.93	0.89	0.78	0.71	0.82	0.75	0.67	0.68	0.73	0.57	0.65	
23/4			0.97	0.95	0.82	0.76	0.85	0.77	0.70	0.72	0.75	0.60	0.68	
3			1.00	1.00	0.85	0.81	0.88	0.80	0.74	0.75	0.77	0.63	0.70	
31/4					0.89	0.86	0.91	0.82	0.77	0.78	0.79	0.66	0.73	
31/2					0.93	0.90	0.94	0.85	0.80	0.81	0.81	0.69	0.75	
33/4					0.96	0.95	0.97	0.87	0.83	0.84	0.83	0.72	0.78	
4					1.00	1.00	1.00	0.90	0.87	0.87	0.84	0.76	0.80	
41/4								0.92	0.90	0.91	0.86	0.79	0.83	
41/2								0.95	0.93	0.94	0.88	0.82	0.85	
43/4								0.97	0.97	0.97	0.90	0.85	0.88	
5								1.00	1.00	1.00	0.92	0.88	0.90	
51/4											0.94	0.91	0.93	
51/2											0.96	0.94	0.95	
53/4											0.98	0.97	0.98	
6		1.00									1.00	1.00	1.00	

See notes below.

#### Edge Distance Shear (f<sub>c</sub>)

	Dia.	3/8		1/2			5/8			3/4			
Edge	Ε	11/2	23/4	3¾	23/4	35/8	53/4	23/4	41/8	53/4	23/4	45/8	53/4
Dist.	Ccr	6	41/2	41/2	6	6	6	71/2	71/2	71/2	9	9	9
c <sub>act</sub> (in.)	Cmin	6	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4
(111.)	f <sub>cmin</sub>	1.00	0.25	0.24	0.25	0.20	0.17	0.19	0.16	0.19	0.19	0.14	0.13
13/4			0.25	0.24	0.25	0.20	0.17	0.19	0.16	0.19	0.19	0.14	0.13
2			0.32	0.31	0.29	0.25	0.22	0.23	0.20	0.23	0.22	0.17	0.16
21/2			0.45	0.45	0.38	0.34	0.32	0.30	0.27	0.30	0.27	0.23	0.22
3			0.59	0.59	0.47	0.44	0.41	0.37	0.34	0.37	0.33	0.29	0.28
31/2			0.73	0.72	0.56	0.53	0.51	0.44	0.42	0.44	0.39	0.35	0.34
4			0.86	0.86	0.65	0.62	0.61	0.51	0.49	0.51	0.44	0.41	0.40
41/2			1.00	1.00	0.74	0.72	0.71	0.58	0.56	0.58	0.50	0.47	0.46
5					0.82	0.81	0.80	0.65	0.63	0.65	0.55	0.53	0.52
51/2					0.91	0.91	0.90	0.72	0.71	0.72	0.61	0.58	0.58
6		1.00			1.00	1.00	1.00	0.79	0.78	0.79	0.66	0.64	0.64
61/2								0.86	0.85	0.86	0.72	0.70	0.70
7								0.93	0.93	0.93	0.78	0.76	0.76
71/2								1.00	1.00	1.00	0.83	0.82	0.82
8											0.89	0.88	0.88
81/2											0.94	0.94	0.94
9											1.00	1.00	1.00

The tabled adjustment values ( $f_c$ ) have been calculated using the following information:

- 1. E = Embedment depth (inches).
- 2.  $C_{act} = \text{actual edge distance at which anchor is installed (inches).}$
- 3.  $c_{cr}$  = critical edge distance for 100% load (inches).
- 4.  $c_{min}$  = minimum edge distance for reduced load (inches).
- $5. f_C = \text{percent of allowable load at actual edge distance.}$
- 6.  $f_{CCT}$  = percentage of allowable load at critical edge distance.  $f_{CCT}$  is always = 1.00.
- f<sub>cmin</sub> = percent of allowable load at minimum edge distance.
- $8.\,f_{c}=f_{cmin}+\left[\left(1-f_{cmin}\right)\left(c_{act}-c_{min}\right)/\left(c_{cr}-c_{min}\right)\right].$

# **Titen HD®** Design Information — Concrete



Load Adjustment Factors for Titen HD® Anchors in Normal-Weight Concrete: Edge Distance, Tension and Shear Loads

#### How to use these charts:

- 1. The following tables are for reduced edge distance.
- Locate the anchor size to be used for either a tension and/or a shear load application.
- Locate the anchor embedment (E) used for either a tension and/or a shear load application.
- 4. Locate the edge distance ( $s_{act}$ ) at which the anchor is to be installed.
- The load adjustment factor (f<sub>s</sub>) is the intersection of the row and column.
- 6. Multiply the allowable load by the applicable load adjustment factor(s).
- 7. Reduction factors for multiple edges are multiplied together.

## Spacing Tension (f<sub>s</sub>)

	Dia.		3/8			1/2			5/8			3/4	
	E	11/2	23/4	3¾	23/4	3%	53/4	23/4	41/8	53/4	23/4	45/8	53/4
s <sub>act</sub> (in)	Scr	4	6	6	8	8	8	10	10	10	12	12	12
(111)	Smin	4	1 1/2	11/2	2	2 2	2	21/2	21/2	21/2	3	3	3
	f <sub>smin</sub>	1.00	0.66	0.56	0.72	0.63	0.76	0.79	0.69	0.73	0.80	0.70	0.72
1													
1½			0.66	0.56									
2			0.70	0.61	0.72	0.63	0.76						
21/2			0.74	0.66	0.74	0.66	0.78	0.79	0.69	0.73			
3			0.77	0.71	0.77	0.69	0.80	0.80	0.71	0.75	0.80	0.70	0.72
4		1.00	0.85	0.80	0.81	0.75	0.84	0.83	0.75	0.78	0.82	0.73	0.75
5			0.92	0.90	0.86	0.82	0.88	0.86	0.79	0.82	0.84	0.77	0.78
6			1.00	1.00	0.91	0.88	0.92	0.89	0.83	0.86	0.87	0.80	0.81
7					0.95	0.94	0.96	0.92	0.88	0.89	0.89	0.83	0.84
8					1.00	1.00	1.00	0.94	0.92	0.93	0.91	0.87	0.88
9								0.97	0.96	0.96	0.93	0.90	0.91
10								1.00	1.00	1.00	0.96	0.93	0.94
11											0.98	0.97	0.97
12											1.00	1.00	1.00

See notes below

# Spacing Shear (f<sub>s</sub>)

	Dia.		3/8			1/2			5/8			3/4	
	E	11/2	23/4	3¾	23/4	3%	53/4	23/4	41/ <sub>8</sub>	53/4	23/4	45/8	53/4
s <sub>act</sub> (in)	Scr	4	0	0	0	0	0	0	0	0	0	0	0
()	Smin	4	0	0	0	0	0	0	0	0	0	0	0
	f <sub>smin</sub>	1.00	0.77	0.77	0.77	0.77	0.77	0.77	0.77	0.77	0.77	0.77	0.77
1													
11/2			0.77	0.77	0.88								
2			0.80	0.80	0.77	0.77	0.77						
21/2			0.82	0.82	0.79	0.79	0.79	0.77	0.77	0.77			
3			0.85	0.85	0.81	0.81	0.81	0.79	0.79	0.79	0.77	0.77	0.77
4		1.00	0.90	0.90	0.85	0.85	0.85	0.82	0.82	0.82	0.80	0.80	0.80
5			0.95	0.95	0.89	0.89	0.89	0.85	0.85	0.85	0.82	0.82	0.82
6			1.00	1.00	0.92	0.92	0.92	0.88	0.88	0.88	0.85	0.85	0.85
7					0.96	0.96	0.96	0.91	0.91	0.91	0.87	0.87	0.87
8					1.00	1.00	1.00	0.94	0.94	0.94	0.90	0.90	0.90
9								0.97	0.97	0.97	0.92	0.92	0.92
10								1.00	1.00	1.00	0.95	0.95	0.95
11											0.97	0.97	0.97
12											1.00	1.00	1.00

The tabled adjustment values  $(f_s)$  have been calculated using the following information:

- 1. E = Embedment depth (inches).
- 2.  $s_{act}$  = actual spacing distance at which anchors are installed (inches).
- 3.  $s_{cr}$  = critical spacing distance for 100% load (inches).
- 4. s<sub>min</sub> = minimum spacing distance for reduced load (inches).
- 5.  $\rm f_{\rm S} = adjustment$  factor for allowable load at actual spacing distance.
- 6.  $f_{SCr}$  = adjustment factor for allowable load at critical spacing distance.  $f_{SCr}$  is always = 1.00.
- f<sub>smin</sub> = adjustment factor for allowable load at minimum spacing distance.
- 8.  $f_s = f_{smin} + [(1 f_{smin}) (s_{act} s_{min}) / (s_{cr} s_{min})].$

# Strong-Tie

SIMPSON

## Simpson Strong-Tie® Anchoring and Fastening Systems for Concrete and Masonry

# **Titen HD®** Design Information — Masonry

## Load-Adjustment Factors for Titen HD® Anchors in Face-of-Wall Installation in 8" Grout-Filled CMU: Edge Distance and Spacing, Tension and Shear Loads

#### How to use these charts:

- 1. The following tables are for reduced edge distance and spacing.
- 2. Locate the anchor size to be used for either a tension and/or shear load application.
- 3. Locate the embedment (E) at which the anchor is to be installed.
- 4. Locate the edge distance (cact) or spacing (sact) at which the anchor is to be installed.
- 5. The load adjustment factor (f<sub>c</sub> or f<sub>s</sub>) is the intersection of the row and column.
- 6. Multiply the allowable load by the applicable load adjustment factor.
- 7. Reduction factors for multiple edges or spacings are multiplied together.

# Edge or End Distance Tension (f<sub>c</sub>)

0			1 0/			
	Dia.	3F8	1/2	5F8	3F4	IBC
	E	41/2	31/2	4 1/2	41/2	
c <sub>act</sub> (in.)	C <sub>C</sub> r	12	12	12	12	
(111.)	C <sub>min</sub>	4	4	4	4	207 852
	f <sub>cmin</sub>	1.00	1.00	0.83	0.66	(33)3
4		1.00	1.00	0.83	0.66	
6		1.00	1.00	0.87	0.75	
8		1.00	1.00	0.92	0.83	(+ +i
10		1.00	1.00	0.96	0.92	
12		1.00	1.00	1.00	1.00	

See notes below

### Edge or End Distance Shear (f<sub>c</sub>) Shear Load Perpendicular to Edge or End (Directed Towards Edge or End)

_	•			,		
	Dia.	3/8	1/2	5/8	3/4	IBC *
_	E	23/4	3 1/2	4 1/2	51/2	
c <sub>act</sub> (in.)	<b>c</b> <sub>cr</sub>	12	12	12	12	<b>→</b>
()	C <sub>min</sub>	4	4	4	4	33 35 S
	f <sub>cmin</sub>	0.58	0.38	0.30	0.21	(22)
4		0.58	0.38	0.30	0.21	
6		0.69	0.54	0.48	0.41	
8		0.79	0.69	0.65	0.61	( <del>-</del>
10		0.90	0.85	0.83	0.80	
12		1.00	1.00	1.00	1.00	

- 1. E = Embedment depth (inches).
- 2. cact = actual end or edge distance at which anchor is installed (inches).
- 3.  $c_{cr}$  = critical end or edge distance for 100% load (inches).
- 4. c<sub>min</sub> = minimum end or edge distance for reduced load (inches).
- $5. f_c =$  adjustment factor for allowable load at actual end or edge distance.
- 6. f<sub>ccr</sub> = adjustment factor for allowable load at critical end or edge distance.  $f_{cor}$  is always = 1.00.
- 7. f<sub>cmin</sub> = adjustment factor for allowable load at minimum end or edge distance.
- 8.  $f_c = f_{cmin} + [(1 f_{cmin}) (c_{act} c_{min}) / (c_{cr} c_{min})].$

#### Spacing Tension (f<sub>c</sub>)

	Dia.	3/8	1/2	5/8	3/4	IB
	E	23/4	31/2	4 1/2	51/2	
s <sub>act</sub> (in.)	Scr	6	8	10	12	1
(111.)	S <sub>min</sub>	3	4	5	6	237
	f <sub>smin</sub>	0.87	0.69	0.59	0.50	(22
3		0.87				
4		0.91	0.69			8
5		0.96	0.77	0.59		14
6		1.00	0.85	0.67	0.50	Carana
8			1.00	0.84	0.67	
10				1.00	0.83	
12					1.00	

- 1. E = Embedment depth (inches).
- 2. sact = actual spacing distance at which anchors are installed (inches).
- 3.  $s_{cr}$  = critical spacing distance for 100% load (inches).
- 4. s<sub>min</sub> = minimum spacing distance for reduced load (inches).
- 5. f<sub>S</sub> = adjustment factor for allowable load at actual spacing distance.
- 6. f<sub>scr</sub> = adjustment factor for allowable load at critical spacing distance, f<sub>scr</sub> is always = 1.00.
- $7.\,f_{\text{Smin}}$  = adjustment factor for allowable load at minimum spacing distance.

### Edge and End Distance Shear (fc) Shear Load Parallel to Edge or End

	Dia.	3/8	1/2	5/8	3/4	I
_	E	23/4	31/2	41/2	41/2	Ŀ
c <sub>act</sub> (in.)	<b>C</b> <sub>C</sub> r	12	12	12	12	
()	Cmin	4	4	4	4	25
	f <sub>cmin</sub>	0.77	0.48	0.46	0.44	6
4		0.77	0.48	0.46	0.44	
6		0.83	0.61	0.60	0.58	
8		0.89	0.74	0.73	0.72	6
10		0.94	0.87	0.87	0.86	
12		1.00	1.00	1.00	1.00	

See notes below

#### Edge or End Distance Shear (f<sub>c</sub>) Shear Load Perpendicular to Edge or End (Directed Away From Edge or End)

	00.00	u.j .		-g	/	
	Dia.	3/8	1/2	5/8	3/4	IBC
_	E	23/4	31/2	4 1/2	51/2	IDO
c <sub>act</sub> (in.)	<b>C</b> <sub>C</sub> r	12	12	12	12	<b>→</b>
(111.)	C <sub>min</sub>	4	4	4	4	X/ 82
	f <sub>cmin</sub>	0.89	0.79	0.58	0.38	(00)0
4		0.89	0.79	0.58	0.38	
6		0.92	0.84	0.69	0.54	
8		0.95	0.90	0.79	0.69	<b>/</b>
10		0.97	0.95	0.90	0.85	
12		1.00	1.00	1.00	1.00	

# oing Choor (f )

Spacin	ig Snea	ar (T <sub>S</sub> )				
	Dia.	3/8	1/2	5/8	3/4	IBC *
	E	23/4	31/2	4 1/2	5 1/2	IDO
s <sub>act</sub> (in.)	Scr	6	8	10	12	-
(111.)	Smin	3	4	5	6	231 ES
	f <sub>smin</sub>	0.62	0.62	0.62	0.62	(22)2
3		0.62				
4		0.75	0.62			n_n
5		0.87	0.72	0.62		<i>I</i> ← →\
6		1.00	0.81	0.70	0.62	
8			1.00	0.85	0.75	
10				1.00	0.87	
12					1.00	

 $\texttt{S.} \ \texttt{Is} = \texttt{Ismin} + \texttt{[(1 - Ismin) (Sact - Smin) / (Scr - Smin)]}.$ 

\* See page 12 for an explanation of the load table icons.

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